

Lpf transfer function

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3rd Loop Transfer Function

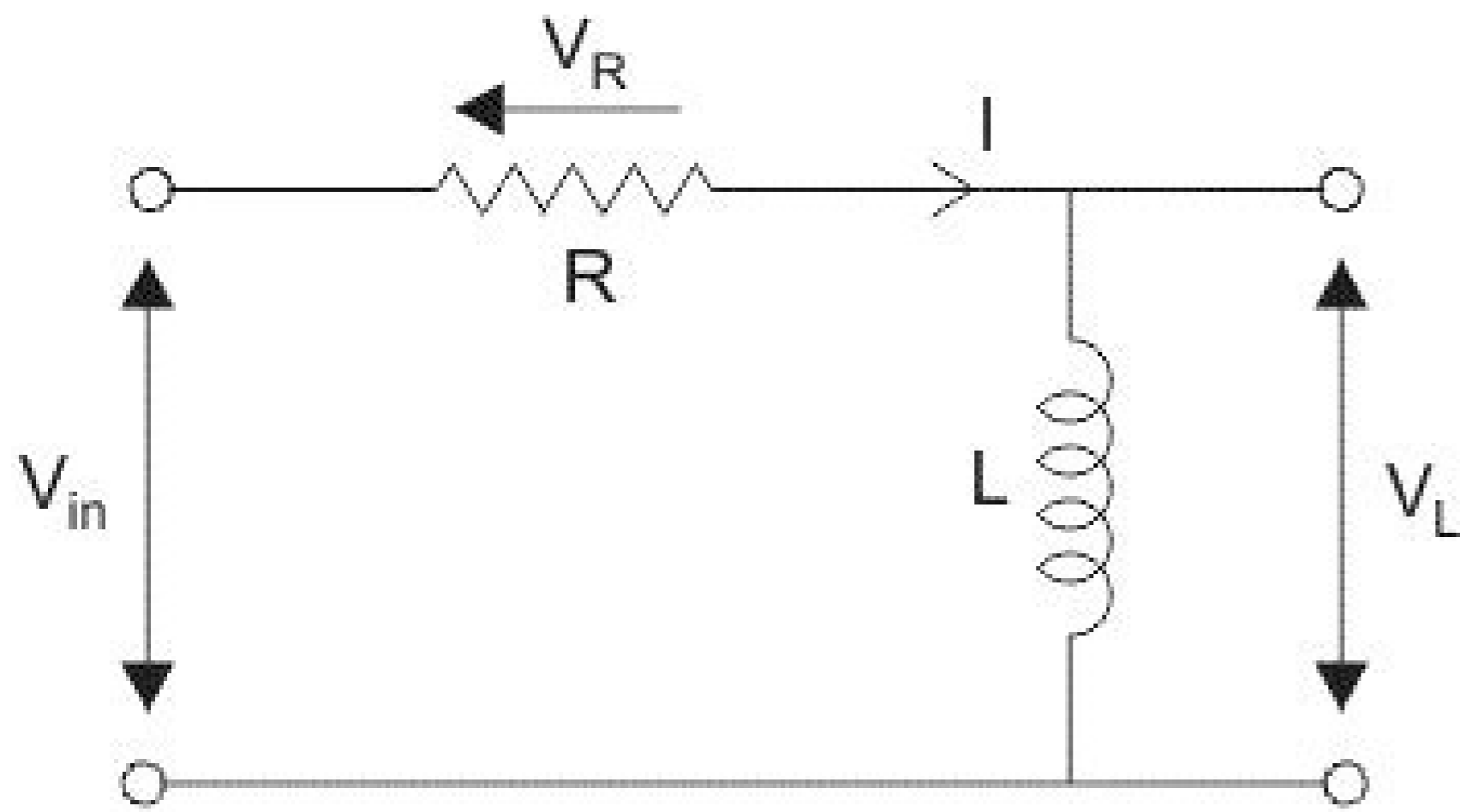
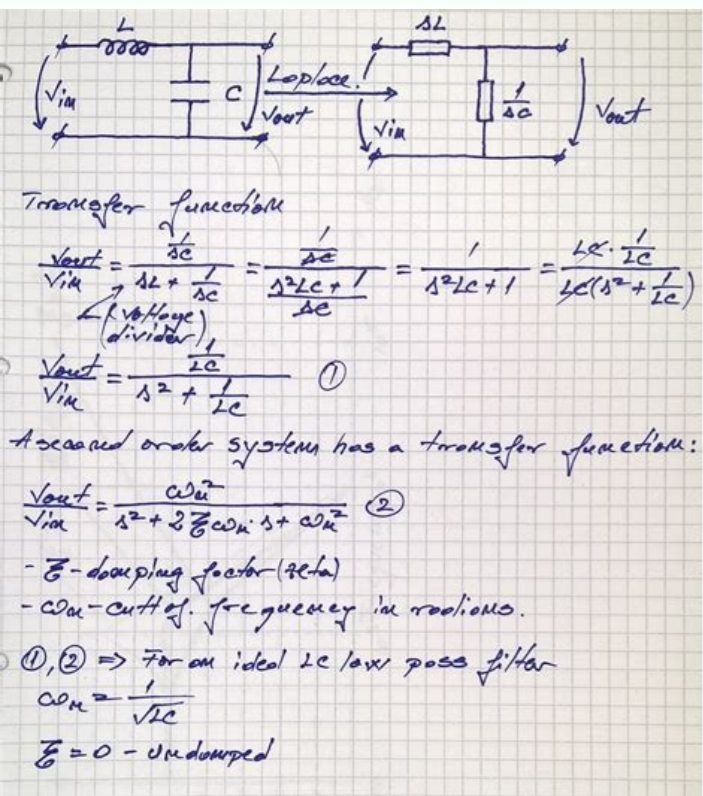
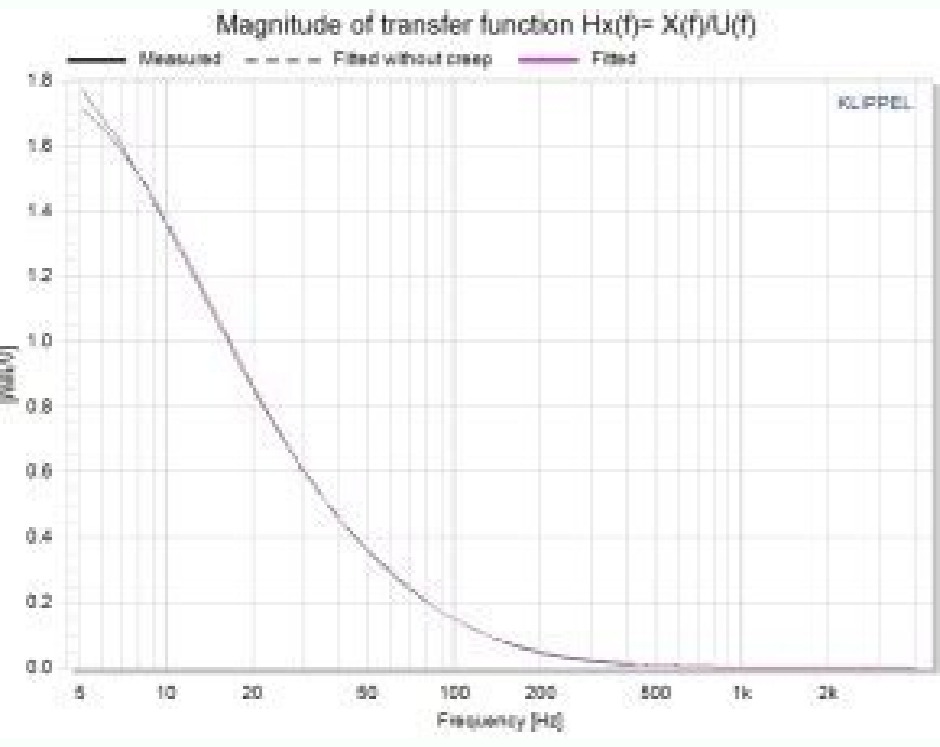
- Using a 2nd order LPF
- Let $m=C_2/C_1$
- Open-loop transfer function

$$G_o(s) = \frac{I_p K_{VCO} (sRC_1 + 1)}{2\pi s^3 RC_1 C_2 + s^2 (C_1 + C_2)} = \frac{I_p K_{VCO} R}{2\pi} \frac{1}{s^3 mRC_1 + s^2 (m+1)}$$

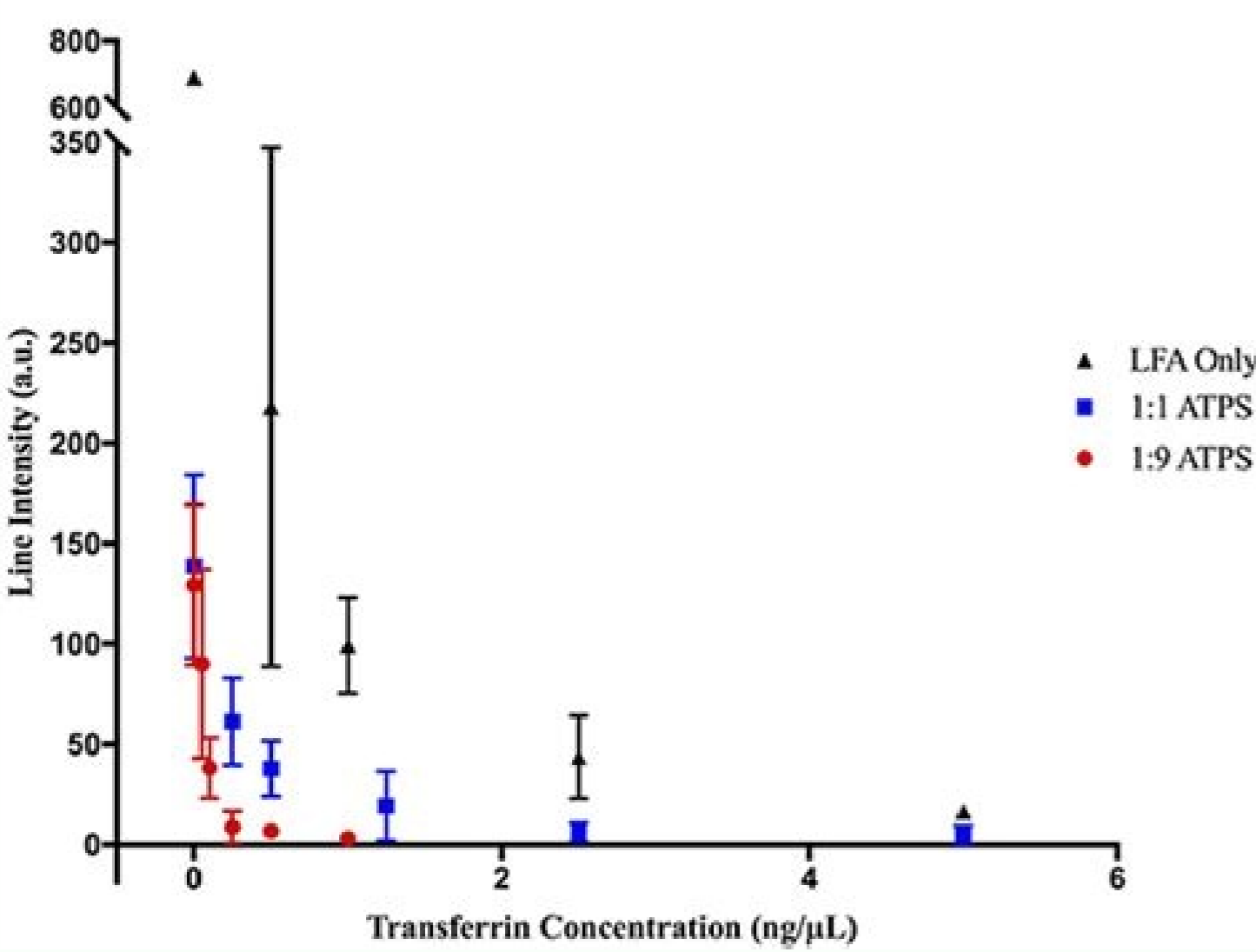
- Closed-loop transfer function

$$G_c(s) = \frac{I_p K_{VCO} R}{2\pi s^3 mRC_1 + s^2 (m+1) + \frac{I_p K_{VCO} R}{2\pi}}$$

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Transferrin Test Line Analysis



Passive high pass filter transfer function. Second order lpf transfer function. High-pass filter transfer function. First order lpf transfer function. Active high pass filter transfer function.

Go to EE494 Index Experiment | 1 | 2 | 3 | ECE Lab Home EE 494 Electrical Engineering Laboratory IV (Part B) Version 1.3 TUTORIAL: Introduction to Filter Design 1.1 Objectives 1.2 Equipment Needed 1.3 References 1.4 Background 1.5 Specifying Butterworth Filters 1.6 Specifying Chebyshev Filters 1.7 Conversion of Specifications 1.8 Examples of Filter Realizations 1.9 Student's Filter Specification 1.1 Objectives In this experiment the student will become familiar with methods used to go from a filter specification to specifying the polynomial transfer function of the filter. Then the student will learn to translate the polynomial transfer function into a working filter design. 1.2 Equipment Needed A decent scientific calculator. A few μ A741 integrated circuit operational amplifiers, resistors and capacitors and a prototyping board. 1.3 References Figure 1.1: A filter specification diagram with a sketch of a Butterworth response that exactly satisfies the specs. 1.4 Background The assignment of designing and building analog filters can be broken up into various tasks. We will assume that the given filter specification is presented in the form shown in figure 1.1. The interpretation of the diagram is the following: It is desired to build a low pass filter whose passband lies in the region $0 \leq f \leq f_p$. The transfer function $|G(f)|$ is almost invariably given in units of dB. Within the passband, the magnitude of the transfer function may vary between zero and G_p . When it enters the stop band, the magnitude of the transfer function should decrease to G_s or less as the frequency f_s is reached. A possible transfer function, in the form of the smooth curve, is shown in figure 1.1. We plan on realizing the filter using a linear analog-circuit. Such circuits have transfer functions whose magnitude squared is an even polynomial in the frequency variable f . Therefore the first step in the design process is to find a polynomial transfer-function that will satisfy the specifications. Many different well-known polynomial transfer-functions are used for approximating filter specifications. Because of time constraints, however, our attention will be confined entirely to Butterworth and Chebyshev polynomial realizations. They have the advantage of having over the years acquired extensive tabulations. But it must be understood at the outset that additional polynomial realizations exist, and that with each is associated a set of advantages and disadvantages which are discussed in the literature. We will now address the question of how to fulfill the specification of the filter by using Butterworth and Chebyshev transfer functions. Back to top EE494 Index 1.5 Specifying Butterworth Filters At the outset we observe that Butterworth filters have the magnitude characteristic given by (1.1) where n is the order of the filter and f_c is the frequency at which the transfer function magnitude is reduced by 3 dB. This class of filters has a monotonically decreasing amplitude characteristic. It has no ripples in the passband, in contrast to Chebyshev and some other filters, and is consequently described as maximally flat. In order to fully specify the filter we need an expression for determining n as well as a method for computing the f_c needed in (1.1). To reach this goal we substitute the filter specifications at f_p and f_s into (1.1) to obtain $1 + (f_p / f_c)^{2n} = 10^{-(G_p / 10)}$ (1.2) $1 + (f_s / f_c)^{2n} = 10^{-(G_s / 10)}$ (1.3) From the last two equations we readily get the two expressions (1.4) (1.5) Taking the ratio of the last two expressions we readily find that (1.6) The example which follows will illustrate the use of the above equations. Example 1: We wish to design a Butterworth filter satisfying $G_p = -1$ dB at $f_p = 3$ kHz and $G_s = -25$ dB at $f_s = 8$ kHz. Substituting the specifications given into (1.6), we obtain the solution (1.7) We need an integer exceeding that given in (1.7), so we fix the value of n at 4. We now simply need to find the value of f_c needed to finish specifying (1.1). Since $n = 4$ exceeds the value of n found in (1.7) we will have some extra latitude in choosing f_c . To find f_c we substitute $n = 4$ into (1.4) and (1.5) to obtain the two equations (1.8) (1.9) The last two equations produce the two results for f_c , $f_{c1} = 3.55$ kHz (1.10) $f_{c2} = 3.90$ kHz (1.11) If we choose a value of f_c somewhere in the range f_{c1}

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